



# Linearization of a coupled system of nonlinear elasticity and fluid

Lorena Bociu, Jean-Paul Zolesio

## ► To cite this version:

| Lorena Bociu, Jean-Paul Zolesio. Linearization of a coupled system of nonlinear elasticity and fluid.  
| [Research Report] Inria. 2009. inria-00442954

**HAL Id: inria-00442954**

**<https://hal.inria.fr/inria-00442954>**

Submitted on 24 Dec 2009

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

# LINEARIZATION OF A COUPLED SYSTEM OF NONLINEAR ELASTICITY AND FLUID

LORENA BOCIU AND JEAN-PAUL ZOLÉSIO

**ABSTRACT.** We model the coupled system formed by an incompressible, irrotational fluid and a nonlinear elastic body. We work with large displacement, small deformation elasticity (or St Venant elasticity), which makes the problem very interesting from the physical point of view. The elastic body is three-dimensional  $\Omega \in \mathbb{R}^3$ , and thus it can not be reduced to its boundary  $\Gamma$  (like in the case of a membrane or a shell). In this paper, we study the static problem, which contrary to common belief, it is more subtle than the dynamical one (since in real life, evolution is more plausible than equilibrium).

## 1. INTRODUCTION

**1.1. The model and the problem.** We consider a model of fluid-structure interaction on a bounded domain  $\mathcal{D} \in \mathbb{R}^3$ . We assume that  $\mathcal{D}$  is comprised of two open domains  $\mathcal{D} = \Omega \cup \Omega^C$ , and has smooth boundary  $\partial\mathcal{D} = \Gamma' \cup \Gamma_{in} \cup \Gamma_{out}$ . The elastic body occupies domain  $\Omega$  with sufficiently smooth boundary  $\Gamma \cup \Gamma'$ , and is described by a nonlinear elastic equation in terms of the displacement  $u$ . The fluid occupies domain  $\Omega^C$  with boundary  $\Gamma \cup \Gamma_{in} \cup \Gamma_{out}$ , and is described by a Navier-Stokes equation in terms of the velocity of the fluid  $v$  and the pressure  $p$ . The interaction takes place on the common boundary  $\Gamma$  and is realized via suitable transmission boundary conditions. We assume that there is a flux  $\vec{f}$  coming into  $\mathcal{D}$  through  $\Gamma_{in}$ , that will determine the velocity of the fluid  $v$  (see Figure 1).

One specific example of the above mentioned model is a 3D tube with elastic walls through which a fluid is flowing. From the physical point of view, this is a very important model with a lot of applications in mathematical biology, more precisely, the study of arterial diseases (the tube represents the artery, the elastic body is the wall of the artery and the fluid is the blood).

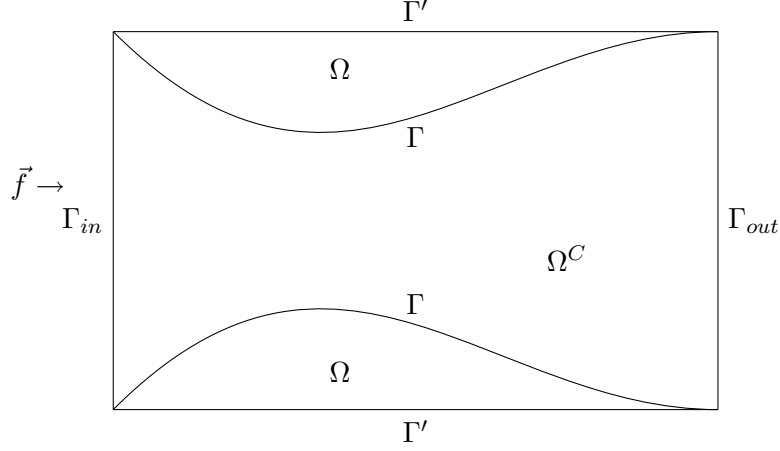
---

*Date:* December 24, 2009.

*2010 Mathematics Subject Classification.* Primary: 35A01, Secondary:

*Key words and phrases.* nonlinear elasticity, Navier-Stokes, linearization, coupled system.

The research of Lorena Bociu was supported by the National Science Foundation under International Research Fellowship OISE-0802187 .



We begin the description of our model by introducing the notation and the basic assumptions on the two equations present in the system.

- **Nonlinear, 3D elasticity:** We work with large displacement, small deformation elasticity (or St Venant elasticity [11]), which makes the problem difficult from the mathematical point of view, and very interesting from the physical point of view. The elastic body is three-dimensional  $\Omega \in \mathbb{R}^3$ , and thus it can not be reduced to its boundary  $\Gamma$  (like in the case of a membrane or a shell).

At rest, the elastic body occupies a reference configuration  $\overline{\mathcal{O}} \in \mathbb{R}^3$ , where  $\mathcal{O}$  is a bounded, open, connected set in  $\mathbb{R}^3$  with sufficiently smooth boundary  $\mathcal{S} \cup \Gamma'$ . When subjected to applied forces, the elastic body occupies a deformed configuration  $\Omega = \varphi(\overline{\mathcal{O}})$ , with smooth boundary  $\Gamma \cup \Gamma'$  (where  $\Gamma'$  is fixed). The deformation of the reference configurations is given by the map  $\varphi : \overline{\mathcal{O}} \rightarrow \mathbb{R}^3$ , that is smooth enough, injective (except possibly on the boundary of the set  $\mathcal{O}$ ), and orientation-preserving (i.e.  $\det \nabla \varphi(x) > 0$ , for all  $x \in \overline{\mathcal{O}}$ ).

Together with the deformation  $\varphi$ , we introduce the displacement  $u : \overline{\mathcal{O}} \rightarrow \mathbb{R}^3$ , defined as usual as  $\varphi = I + u$ , where  $I$  denotes identity map  $I : \overline{\mathcal{O}} \rightarrow \mathbb{R}^3$ .

It is well known that a body occupying a deformed configuration  $\overline{\Omega}$ , and subjected to zero applied body forces in its interior  $\Omega$  and to applied surface forces on the boundary  $\Gamma$ , is in static equilibrium if the fundamental stress principle of Euler and Cauchy is satisfied:

$$\begin{cases} -\operatorname{div} \mathcal{T} = 0 & \text{in } \Omega \\ \mathcal{T} n^\varphi = g^\varphi & \text{on } \Gamma \end{cases} \quad (1.1)$$

where  $\hat{g}$  represents the density of the applied surface force,  $n^\varphi$  is the unit outer normal vector along  $\Gamma$ , and the tensor  $\mathcal{T}$  is the Cauchy stress tensor. The above equilibrium equations over  $\overline{\Omega}$  are equivalent to the equilibrium

equations over the reference configuration  $\overline{\mathcal{O}}$ :

$$\begin{cases} -\operatorname{div} \mathcal{P} = 0 & \text{in } \mathcal{O} \\ \mathcal{P}n = g & \text{on } \mathcal{S} \end{cases} \quad (1.2)$$

where  $n$  denotes the unit outer normal vector along  $\mathcal{S}$ ,  $gda = \hat{g}da^\varphi$ , and  $\mathcal{P} : \overline{\mathcal{O}} \rightarrow \mathbb{M}^3$  is the Piola transform of the Cauchy stress tensor field, defined by

$$\mathcal{P}(x) = \mathcal{T}(x^\varphi) \operatorname{Cof} \nabla T(x) = \det(\nabla \varphi(x)) \mathcal{T}(x^\varphi) (\nabla \varphi)^{-*} \quad (1.3)$$

From the constitutive equations, we have that  $\mathcal{P}(x) = \nabla \varphi(x) \Sigma(u(x))$ , where  $\Sigma$  defines the second Piola-Kirchhoff stress tensor. In terms of the displacement  $u$ ,  $\Sigma$  is given by

$$\Sigma(\sigma(u)) = \lambda(\operatorname{tr} \sigma(u))I + 2\mu\sigma(u) \quad (1.4)$$

where  $\lambda$  and  $\mu$  are the Lamé constants of the material, and the Green-St Venant strain tensor  $\sigma(u)$  is given by

$$\sigma(u) = \frac{1}{2}(Du^* + Du + Du^*Du) \quad (1.5)$$

Therefore equations (1.2) can be rewritten as

$$\begin{cases} -\operatorname{div}[(I + \nabla u)\Sigma(\sigma(u))] = 0 & \text{in } \mathcal{O} \\ (I + \nabla u)\Sigma(\sigma(u))n = g & \text{on } \mathcal{S} \end{cases} \quad (1.6)$$

The advantage of the equilibrium equations over the reference configuration (1.2) or (1.6) over (1.1) is the fact that they are written in terms of the Lagrange variable  $x$  that is attached to the reference configuration, instead of the Euler variable  $x^\varphi = \varphi(x)$ , which is precisely one of the unknowns.

Nevertheless, we want to stress the fact that equations (1.1) play a critical role when dealing with elastic body - fluid systems, where the coupling is taking place on the boundary interface between the two media. This interface is precisely the boundary  $\Gamma$  of the deformed configuration of the elastic body  $\Omega$  and thus the coupling requires the continuity of the velocities and the normal stress tensors across  $\Gamma$ . Therefore, we need a relationship between the Cauchy stress tensor  $\mathcal{T}$  and the strain tensor  $\sigma(u)$ , that will provide us with the correct matching of the two dynamics on the common interface.

Recalling the relations between  $\mathcal{P}$ ,  $\mathcal{T}$ , and  $\Sigma(u)$  we obtain that

$$\mathcal{T} = \left( \frac{1}{\det(\nabla \varphi)} \nabla \varphi \cdot \Sigma(\sigma(u)) \cdot (\nabla \varphi)^* \right) \circ \varphi^{-1} \quad (1.7)$$

• **Potential fluid:** We assume that the fluid present in the system is incompressible and irrotational. This means that the fluid is a potential fluid  $v = \nabla \phi$ , where  $v$  is the velocity of the fluid and  $\phi$  (the velocity potential of the fluid) satisfies the Laplace equation  $\Delta \phi = 0$  (due to the incompressibility condition which translates into  $\nabla \cdot u = 0$ ).

Now if  $p$  represents the pressure of the fluid and  $\eta$  the viscosity, then the flow is described by the following Navier-Stokes equation

$$v \cdot \nabla v - \eta \Delta v + \nabla p = \rho \vec{g} \quad (1.8)$$

where  $\rho$  is the density, and  $\vec{g}$  is the gravitational acceleration. Due to the fluid being irrotational (vorticity  $\text{curl } v = 0$ ), the convective acceleration reduces to  $v \cdot \nabla v = \nabla \left( \frac{\|v\|^2}{2} \right)$  and thus (1.8) becomes

$$\nabla \left( \frac{1}{2} \|\nabla \phi\|^2 + p - \rho g z \right) = 0$$

This provides us with the formula for the pressure  $p$  of the fluid:

$$p = c + \frac{1}{2} \|\nabla \phi\|^2 - \rho g z \quad (1.9)$$

**1.2. Fluid-structure interaction: the mathematical model.** Now we couple the two dynamics described above and we require continuity of both the velocities and the normal stress tensors across the common boundary  $\Gamma$ . Recall that  $\mathcal{D} = \Omega \cup \Omega^C$ , with boundary  $\partial \mathcal{D} = \Gamma' \cup \Gamma_{in} \cup \Gamma_{out}$ , the elastic body occupies domain  $\Omega$ , and the fluid occupies  $\Omega^C$  (see Figure 1).

We obtain the following PDE model in variables  $(\phi, u)$ :

$$\begin{cases} \Delta \phi = 0 & , \Omega^C \\ -\text{div}(\mathcal{T}) = 0 & , \Omega \\ \nabla \phi \cdot n = 0 & , \Gamma \\ \mathcal{T} \cdot n = (c + \frac{1}{2} \|\nabla \phi\|^2 - \rho g z) n & , \Gamma \\ u = 0 & , \Gamma' \end{cases} \quad (1.10)$$

where  $n$  is the unit outer normal vector along  $\Gamma$ , and  $f$  is the flux coming in  $\mathcal{D}$  through  $\Gamma_{in}$ . Recall that  $\mathcal{T}$  is the Cauchy stress tensor, given by

$$\mathcal{T} = \left( \frac{1}{\det(\nabla \varphi)} \nabla \varphi \cdot \Sigma(\sigma(u)) \cdot (\nabla \varphi)^* \right) \circ \varphi^{-1}$$

Thus the two equations on  $\Gamma$  present in (1.10) are equivalent to

$$\begin{cases} \nabla \phi \cdot n = 0 & , \text{ on } \Gamma \\ \frac{1}{\det(\nabla \varphi)} \nabla \varphi \cdot \Sigma(\sigma(u)) \cdot (\nabla \varphi)^* \cdot n \circ \varphi = [(c + \frac{1}{2} \|\nabla \phi\|^2 - \rho g z) n] \circ \varphi & , \text{ on } \Gamma \end{cases} \quad (1.11)$$

**1.2.1. Boundary conditions on  $\Gamma_{in}$ .** Now we describe the flow (which so far we called  $f$ ) coming into the domain through  $\Gamma_{in}$ . Let  $c(x)$  be a given, smooth function defined on  $\Gamma_{in}$  such that

$$\begin{cases} c(x) = 0 & \text{ on } \partial \Gamma_{in}, \\ \frac{\partial}{\partial n} \phi = c(x) & \text{ on } \Gamma_{in} \end{cases} \quad (1.12)$$

Then it follows that

$$0 = \int_{\Omega^c} \operatorname{div}(\nabla \phi) dx = \int_{\Gamma_{in}} \frac{\partial \phi}{\partial n_{in}} d\Gamma_{in} + \int_{\Gamma_{out}} \frac{\partial \phi}{\partial n_{out}} d\Gamma_{out} \quad (1.13)$$

At this point, we choose  $\alpha \in \mathbb{R}$  verifying

$$\begin{cases} \alpha = \frac{\partial \phi}{\partial n_{out}} & \text{on } \Gamma_{out}, \\ \int_{\Gamma_{out}} \alpha d\Gamma_{out} = - \int_{\Gamma_{in}} c(x) d\Gamma_{in} \end{cases} \quad (1.14)$$

## 2. DESCRIPTION OF THE STATIC PROBLEM

**2.1. Parameter of Perturbation  $s$ .** As previously mentioned, in this paper we are interested in the static problem associated with system (1.10). In a subsequent paper, we will consider the dynamical case. Contrary to common belief, the steady problem is more subtle than the dynamical one, since in real life, evolution is more plausible than equilibrium.

We assume that the flux entering the domain  $\mathcal{D}$  is dependent on a parameter of perturbation  $s$ , i.e.  $c(x)$  is a given, smooth function defined on  $\Gamma_{in}$  such that

$$\begin{cases} c(x) = 0 & \text{on } \partial\Gamma_{in}, \\ \frac{\partial}{\partial n} \phi_s = (1+s)c(x) & \text{on } \Gamma_{in} \end{cases} \quad (2.1)$$

Then it follows that

$$0 = \int_{\Omega_s^c} \operatorname{div}(\nabla \phi_s) dx = \int_{\Gamma_{in}} \frac{\partial \phi_s}{\partial n_{in}} d\Gamma_{in} + \int_{\Gamma_{out}} \frac{\partial \phi_s}{\partial n_{out}} d\Gamma_{out} \quad (2.2)$$

For any  $s \geq 0$ , we choose  $\alpha_s \in \mathbb{R}$  verifying

$$\begin{cases} \alpha_s = \frac{\partial \phi_s}{\partial n_{out}} & \text{on } \Gamma_{out}, \\ \int_{\Gamma_{out}} \alpha d\Gamma_{out} = -(1+s) \int_{\Gamma_{in}} c(x) d\Gamma_{in}, & \text{for all } s \geq 0 \end{cases} \quad (2.3)$$

If the elastic body occupies a reference configuration  $\overline{\mathcal{O}} \in \mathbb{R}^3$  with smooth boundary  $\mathcal{S} \cup \Gamma'$ , then, when subjected to applied forces, it occupies a deformed configuration  $\Omega_s = \varphi_s(\overline{\mathcal{O}})$ , with smooth boundary  $\Gamma_s \cup \Gamma'$  (where  $\Gamma'$  is fixed). The deformation map in this case is dependant on the parameter  $s$ :  $\varphi_s : \overline{\mathcal{O}} \rightarrow \mathbb{R}^3$ , but nevertheless is smooth enough, injective, and orientation-preserving. The displacement  $u_s : \overline{\mathcal{O}} \rightarrow \mathbb{R}^3$  becomes  $u_s = \varphi_s - I$ , where  $I$  is the identity map  $I : \overline{\mathcal{O}} \rightarrow \mathbb{R}^3$ .

Similarly, for the fluid present in the system, its velocity and pressure are now functions of  $s$ :  $v_s = \nabla \phi_s$ , and  $p_s = c_s + \frac{1}{2} \|\nabla \phi_s\|^2 - \rho g z$ .

Therefore we are interested in the following PDE model:

$$\begin{cases} \Delta \phi_s = 0 & , \Omega_s^C \\ -\operatorname{div}(\mathcal{T}_s) = 0 & , \Omega_s \\ \nabla \phi_s \cdot n_s = 0 & , \Gamma_s \\ \mathcal{T}_s \cdot n_s = (c_s + \frac{1}{2} \|\nabla \phi_s\|^2 - \rho g z) n & , \Gamma_s \\ u = 0 & , \Gamma' \\ \int_{\Gamma_{out}} \alpha \, d\Gamma_{out} = -(1+s) \int_{\Gamma_{in}} c(x) \, d\Gamma_{in}, \text{ for all } s \geq 0 \end{cases} \quad (2.4)$$

where  $n_s$  is the unit outer normal vector along  $\Gamma_s$ ,  $\mathcal{T}_s$  is the Cauchy stress tensor (associated to  $s$ ), given by

$$\mathcal{T} = \left( \frac{1}{\det(\nabla \varphi_s)} \nabla \varphi_s \cdot \Sigma(\sigma(u_s)) \cdot (\nabla \varphi_s)^* \right) \circ \varphi_s^{-1} \quad (2.5)$$

and the boundary conditions are equivalent to

$$\begin{cases} \nabla \phi_s \cdot n_s = 0 & , \text{ on } \Gamma_s \\ \frac{1}{\det(\nabla \varphi_s)} \nabla \varphi_s \cdot \Sigma(\sigma(u_s)) \cdot (\nabla \varphi_s)^* \cdot n_s \circ \varphi_s = [(c_s + \frac{1}{2} \|\nabla \phi_s\|^2 - \rho g z) n_s] \circ \varphi_s & , \text{ on } \Gamma_s \end{cases} \quad (2.6)$$

Our goal is to study, for any given value of  $s$ , the equilibrium problem associated with the coupled system (2.4).

**2.2. The moving boundary  $\Gamma_s$ .** Recall that the deformation map  $\varphi$  maps the reference boundary  $\mathcal{S}$  to  $\Gamma$ . Similarly, the deformation  $\varphi_s$  associated with  $\hat{f} = f + s$  maps  $\mathcal{S}$  to  $\Gamma_s$ .

At this point it is convenient to introduce the map  $T_s : \Gamma \rightarrow \Gamma_s$  that builds the moving boundary  $\Gamma_s$ :

$$T_s = \varphi_s \circ \varphi^{-1} \quad (2.7)$$

and the speed  $V(s, \cdot)$  associated with the flow mapping  $T_s$ :

$$V(s, \cdot) = \left( \frac{\partial}{\partial s} T_s \right) \circ T_s^{-1} = \frac{\partial}{\partial s} \varphi_s \circ \varphi_s^{-1} \quad (2.8)$$

This means that  $T_s(V) : X \rightarrow x(s)$ , where  $x(s)$  satisfies the following differential equation

$$\begin{cases} \frac{\partial}{\partial s} x = V(s, x(s)) \\ x(0) = X \end{cases} \quad (2.9)$$

which is equivalent to  $x(s) = X + \int_0^s V(t, x(t)) dt$ .

**2.2.1. Transport of scalar operators.** Let  $D$  be a bounded domain in  $R^N$  and  $T$  be a one-to-one transformation from  $D$  onto  $\bar{D}$  and from  $\bar{D}$  onto  $D$ . Let  $S = T^{-1}$  be the inverse mapping. As  $T \circ S = I$ , we obtain that  $DT \circ S \cdot DS = I$ , and therefore

$$DS = (DT)^{-1} \circ S,$$

and

$$(DS) \circ T = (DT)^{-1}.$$

For any  $\phi \in H^1(D)$  we have

$$(\nabla \phi) \circ T = (DT)^{-*} \cdot \nabla(\phi \circ T)$$

We also have:

$$\begin{aligned} \frac{d}{ds} T_s &= V(s) \circ T_s \Rightarrow \frac{d}{ds} T_s \Big|_{s=0} = V(0). \\ \frac{d}{ds} DT_s(X) &= DV(s, T_s(X)) DT_s(X), \quad DT_0(X) = I \\ \Rightarrow \frac{d}{ds} DT_s \Big|_{s=0} &= DV(0) \quad \text{and} \quad \frac{d}{ds} (DT_s)^{-1} \Big|_{s=0} = -DV(0). \\ \frac{d}{ds} \det DT_s(X) &= \text{tr} DV(s, T_s(X)) \det DT_s(X) = \text{div} V(s, T_s(X)) \det DT_s(X), \\ \Rightarrow \frac{d}{ds} \det(DT_s) \Big|_{s=0} &= \text{div} V(0). \end{aligned}$$

Now let  $\vec{E}$  be a  $C^1$  vector field defined over  $D$ . Then we have the following property:

**Property 2.1.**

$$(\text{div} E) \circ T = \det(DT)^{-1} \text{div}(\det(DT) (DT)^{-1} \cdot (E \circ T))$$

*Proof.* Let  $\phi \in C_{comp}^\infty(D)$ . Using the change of variable  $y = T(x)$  (or  $x = S(y)$ ), we obtain:

$$\begin{aligned} \int_D (\text{div} E) \circ T(x) \phi(x) dx &= \int_D \text{div} E(y) \phi \circ S(y) \det(DS)(y) dy \\ &= - \int_D \langle E(y), \nabla(\phi \circ S(y) \det(DS)(y)) \rangle dy \\ &= - \int_D \langle E(y), \nabla(\phi \circ S(y)) \det(DS)(y) \rangle + \phi \circ S(y) \nabla(\det(DS)(y)) \rangle dy \\ &\quad [\text{Using the identity } \nabla(\phi \circ S) = (DS)^* \cdot (\nabla \phi) \circ S, \text{ we obtain:}] \\ &= - \int_D \langle E(y), (DS)^* \cdot (\nabla \phi) \circ S \det(DS)(y) \rangle + \phi \circ S(y) \nabla(\det(DS)(y)) \rangle dy \\ &\quad [\text{Transposing of the matrix } DS^*, \text{ we can rewrite as follows:}] \\ &= - \int_D \{ \langle \det(DS)(y) \rangle DS \cdot E(y), (\nabla \phi) \circ S \rangle + \langle \nabla(\det(DS)(y)) E(y), \phi \circ S(y) \rangle \} dy \\ &\quad [\text{Performing the change of variable } y = T(x), \text{ we obtain:}] \\ &= - \int_D \{ \langle \det(DT) \det(DS) \circ T DS \circ T \cdot E \circ T, \nabla \phi \rangle + \langle \det(DT) (\nabla \det(DS)) \circ T E \circ T, \phi \rangle \} dx \\ &\quad [\text{As } (DS) \circ T = (DT)^{-1} \Rightarrow \det(DS) \circ T = \det((DS) \circ T) = \det((DT)^{-1}) = \\ &\quad (\det DT)^{-1}, \text{ then we have:}] \end{aligned}$$



$$\begin{aligned}
&= - \int_D \{ \langle (DT)^{-1}.E \circ T, \nabla \phi \rangle + \langle \det(DT)(\nabla \det(DS)) \circ T E \circ T, \phi \rangle \} dx \\
&\quad [\text{Using the fact that } (\nabla \det(DS)) \circ T = (DT)^{-*}.\nabla(\det(DS) \circ T) = (DT)^{-*}.\nabla(\frac{1}{\det DT})] \\
&= - \frac{1}{(\det DT)^2} (DT)^{-*}.\nabla(\det DT), \text{ we obtain:}] \\
&= - \int_D \{ \langle (DT)^{-1}.E \circ T, \nabla \phi \rangle - \langle \det(DT)^{-1} (DT)^{-*}.\nabla(\det DT).E \circ T, \phi \rangle \} dx \\
&= \int_D \{ \text{div}((DT)^{-1}.E \circ T) + \det(DT)^{-1} \langle (DT)^{-*}.\nabla(\det DT), E \circ T \rangle \} \phi dx \\
&= \int_D \{ \text{div}((DT)^{-1}.E \circ T) + \det(DT)^{-1} \langle \nabla(\det DT), (DT)^{-1}.E \circ T \rangle \} \phi dx \\
&= \int_D \det(DT)^{-1} \{ \det(DT) \text{div}((DT)^{-1}.E \circ T) + \langle \nabla(\det DT), (DT)^{-1}.E \circ T \rangle \} \phi dx \\
&\quad [\text{For any scalar function } a \text{ and any vector function } \vec{A} \text{ we have } \text{div}(a \vec{A}) = a \text{div} \vec{A} + \langle \nabla a, \vec{A} \rangle_{\mathbb{R}^3}. \text{ Therefore we have that } \det(DT) \text{div}((DT)^{-1}.E \circ T) + \langle \nabla(\det DT), (DT)^{-1}.E \circ T \rangle = \text{div}(\det(DT) (DT)^{-1}.E \circ T), \text{ which gives us the desired conclusion:}]
\end{aligned}$$

$$= \int_D \det(DT)^{-1} \text{div}(\det(DT) (DT)^{-1}.E \circ T) \phi dx$$

□

Similarly, we can prove the following proposition:

**Property 2.2.** *For any  $\phi \in H^1(D)$ , we have the following identity:*

$$\Delta \phi \circ T = \det(DT)^{-1} \text{div}(\det(DT)(DT)^{-1}(DT)^{-*} \nabla(\phi \circ T)) \quad (2.10)$$

**2.2.2. Transport of Vector Operators.** Let  $\mathcal{T}$  be a  $N \times N$  matrix function defined on  $D$ . We consider the vector Divergence operator  $\text{Div} \vec{\mathcal{T}}$  being defined as the vector whose  $i^{\text{th}}$  component is the (scalar) divergence of the vector composed of the  $i^{\text{th}}$  line of the matrix  $\mathcal{T}$ :

$$(\text{Div} \vec{\mathcal{T}})_i = \text{div}(\mathcal{T}_{i,\cdot}) = \sum_{j=1,\dots,N} \frac{\partial}{\partial x_j} \mathcal{T}_{i,j}$$

From the previous section we obtain that

$$((\text{Div} \vec{\mathcal{T}}) \circ T)_i = (\text{Div} \vec{\mathcal{T}})_i \circ T = \det(DT)^{-1} \text{div}(\det(DT) (DT)^{-1}(\mathcal{T}_{i,\cdot}) \circ T)$$

It turns out that  $(\mathcal{T}_{i,\cdot}) \circ T$  is the  $i^{\text{th}}$  column vector of the matrix  $\mathcal{T}^* \circ T$  so that  $(DT)^{-1}(\mathcal{T}_{i,\cdot}) \circ T$  is the  $i^{\text{th}}$  column of the matrix  $(DT)^{-1} \mathcal{T}^* \circ T$ , and thus the  $i^{\text{th}}$  line of the matrix  $(DT)^{-1} \mathcal{T} \circ T$ . Therefore we have the following identity:

**Property 2.3.**

$$(\text{Div} \vec{T}) \circ T = \det(DT)^{-1} \text{Div}(\det(DT) (DT)^{-1} \cdot (\mathcal{T} \circ T))$$

**2.2.3. Boundary change of variable.** Let  $\Gamma = \partial\Omega$  be a  $C^1$  manifold: there exists a covering  $\Gamma \subset \cup_{i=1,\dots,M} \mathcal{O}_i$ , open subsets and charts  $c_i : \mathcal{O}_i \rightarrow B$  where  $B$  is the unit ball of  $R^N$  such that  $c_i(\Gamma \cap \mathcal{O}_i) \subset B_0 = \{x = (x', 0) \in B\}$  and  $c_i(\Omega \cap \mathcal{O}_i) \subset B + 0 = \{x = (x', z) \in B \text{ s.t. } z > 0\}$ . Let  $r_i \in C^\infty(D)$  with compact support in  $\mathcal{O}_i$  such that  $0 \leq r_i \leq 1$ ,  $\sum r_i = 1$  in a neighbourhood of the boundary  $\Gamma$ . For any  $f \in L^1(\Gamma)$  we have

$$\begin{aligned} \int_{\Gamma} f d\Gamma &= \sum \int_{\Gamma \cap \mathcal{O}_i} r_i f d\Gamma \\ &= \sum \int_{B_0} r_i \circ c_i^{-1} f \circ c_i^{-1} \|\text{cof}(D(c_i^{-1})).n_0\| dx' \end{aligned}$$

Where for any square matrix  $A$ , the cofactor's matrix is

$$\text{cof}(A) = \det A \quad A^{-*}, \quad \text{cof}(A^{-1}) = \frac{1}{\det A} A^*$$

We get  $D(c_i^{-1}) = (Dc_i)^{-1} \circ c_i^{-1}$  then

$$\text{cof}(D(c_i^{-1})) = \text{cof}((Dc_i)^{-1}) \circ c_i^{-1} = \left( \frac{1}{\det Dc_i} (Dc_i)^* \right) \circ c_i^{-1}$$

It can be easily verified that if  $T$  is a smooth enough transformation we have, with  $\Sigma = T(\Gamma)$ ,

$$\int_{T(\Gamma)} f d\Sigma = \int_{\Gamma} f \circ T \omega d\Gamma$$

Where,  $n$  being the unitary normal field on  $\Gamma$ ,

$$\omega = \|\text{cof}(DT).n\| = |\det(DT)| \|(DT)^{-*}.n\|$$

Also, we have the following lemma ([15]):

**Lemma 2.1.** *If the mapping  $s \rightarrow T_s(V)$  is in  $C^1([0, \tau]; C^k(\overline{D}, \mathbb{R}^n))$ , then*

$$s \rightarrow n_s \circ T_s = \frac{DT_s^{-*} n}{\|DT_s^{-*} n\|} \text{ is in } C^1([0, \tau]; C^k(\Gamma))$$

where  $n$  and  $n_s$  are the outward normal fields respectively to  $\Omega$  and  $\Omega_s$ , on  $\Gamma$  and  $\Gamma_s$ . Moreover, its derivative is given by:

$$\frac{d}{ds}(n_s \circ T_s) = \langle DV \cdot n_s, n_s \rangle \circ T_s n_s \circ T_s - DV^* \circ T_s n_s \circ T_s$$

**2.2.4. Shape derivatives.** Assume that the transformation under consideration  $T_s(V)$  is the flow mapping of a Lipschitz-continuous vector field  $V(s, x)$ . Then we get

$$\forall x \in \Gamma, \omega(s, x) = \det(DT_s(V)) \|(DT_s(V))^{-*}.n\|$$

and

$$\forall x \in \Gamma, \frac{\partial}{\partial s} \omega(s, x)|_{s=0} = H(x) \cdot \langle V(0, x), n(x) \rangle$$

Where  $H$  is the mean curvature of  $\Gamma$ ,  $H = \text{Trace}(D^2 b_\Omega)|_\Gamma = (\Delta b_\Omega)|_\Gamma$  and  $v = \langle V(0, x), n(x) \rangle$  is the so-called normal speed of the moving boundary  $\Gamma_s$ .

### 3. MATERIAL DERIVATIVES

**3.1. Existence results for the derivative.** Recall that  $\mathcal{O}$  is the reference domain whose boundary is  $S$  and let  $\mathcal{O}^c$  be its complementary. The mapping  $I + u_s$  is invertible from  $\mathcal{O}$  onto  $\Omega_s$  as soon as  $\det(I + Du_s) > 0$  over  $\mathcal{O}$ . We transport the harmonic problem whose solution is  $\phi_s \in H^1(\Omega_s)$ . Let

$$\phi^s := \phi_s \circ (I + u_s) \in H^1(\hat{\Omega})$$

From the Transport Lemma we know that

$$\text{div}(A(s). \nabla \phi^s) = 0 \text{ in } \mathcal{O}^c \quad (3.1)$$

where

$$A(s) = \det(I + Du_s) (I + Du_s)^{-1} \cdot (I + Du_s)^{-*}$$

Moreover, we have the following boundary condition

$$\langle \hat{n}, A(s). \nabla \phi^s \rangle = 0 \text{ on } S \quad (3.2)$$

Concerning the elastic boundary condition on  $\Gamma_s$ , we have:

$$\mathcal{T}_s.n_s = \frac{1}{2} |\nabla_{\Gamma_s} \phi_s|^2 + f \text{ on } \Gamma_s \quad (3.3)$$

where the forcing term  $f$ , may be due to the gravity acceleration and can take the form  $f(x) = \rho g x_3$  in  $R^3$ . The change of variable leads to

$$\mathcal{T}_s \circ (I + u_s).n_s \circ (I + u_s) = \frac{1}{2 \det(I + Du_s)} \langle A(s). \nabla \phi^s, \nabla \phi^s \rangle + f \circ (I + u_s) \text{ on } \Gamma_s \quad (3.4)$$

The stress tensor is the matrix

$$\mathcal{T}_s \circ (I + u_s) = \left( \frac{1}{\det(I + Du_s)} (I + Du_s). \Sigma(\sigma(u_s)). (I + D^* u_s) \right) \quad (3.5)$$

Where

$$\Sigma(\sigma(u_s)) = C_{\lambda, \mu} \cdot (Du_s + D^* u_s + \frac{1}{2} Du_s \cdot D^* u_s) \quad (3.6)$$

$$n_s \circ (I + u_s) = (I + Du_s)^{-*} \cdot \nabla (b_{\Omega_s} \circ (I + u_s))$$

Equation (3.1), (3.2), (3.3), (3.4), and (3.5) above form a system that we can rewrite as

$$\mathcal{F}(s, (u_s, \phi^s)) = 0,$$

where the mapping

$$\mathcal{F} : [0, s_1[ \times (H^1(\hat{\Omega}, R^N) \times H^1(\hat{\Omega})) \rightarrow H^{-1}(\hat{\Omega}, R^N) \times H^{-1}(\hat{\Omega})$$

verifies the Implicit Function theorem assumptions so that the derivative  $u' := \frac{\partial}{\partial s} u_s|_{s=0}$  exists in  $H^1(\hat{\Omega}, R^N)$  and also  $\dot{\phi} := \frac{\partial}{\partial s} \phi^s|_{s=0}$  exists in  $H^1(\hat{\Omega}, R)$ .

#### 4. WEAK FORMULATION OF THE PROBLEM

Now we write the variational form associated with system (2.4).  $\forall \Psi \in H^1(D)$ ,  $\forall R \in H^1(D, R^N)$ , we have

$$\begin{aligned} & \int_{\Omega_s} \text{Tr}(\mathcal{T}_s \cdot DR) dx + \int_{\Omega_s^c} \langle \nabla \phi_s, \nabla \Psi \rangle dx \\ &= \int_{\Gamma_s} \left\{ \frac{1}{2} |\nabla \phi_s|^2 + \rho g x_3 \right\} \langle n_s, R \rangle d\Gamma_s \end{aligned}$$

Our goal is to compute the  $s$  derivatives (at  $s = 0$ ). Let  $\mathcal{T}' = [\frac{\partial}{\partial s} \mathcal{T}_s]_{s=0}$ ,  $v = \langle V(0), n \rangle$  on  $\Gamma$ , and  $n' = \frac{d}{ds} (\nabla b_{\Omega_s})_{s=0}$ . Recall that  $n_s = \nabla b_{\Omega_s}$  is the unit normal vector field on  $\Gamma_s$  out going to the (elastic) set  $\Omega_s$ , and  $H = \Delta b_{\Omega}$  is the mean curvature of  $\Gamma$ . We obtain:

$$\begin{aligned} & \int_{\Omega} \text{Tr}(\mathcal{T}' \cdot DR) dx + \int_{\Gamma} \text{Tr}(\mathcal{T} \cdot DR) v d\Gamma \\ &+ \int_{\Omega^c} \langle \nabla \phi', \nabla \Psi \rangle dx + \int_{\Gamma} \langle \nabla \phi, \nabla \Psi \rangle v d\Gamma \\ &= \int_{\Gamma} \{ \langle \nabla \phi', \nabla \phi \rangle \langle n, R \rangle d\Gamma \\ &+ \int_{\Gamma} \left\{ \frac{1}{2} |\nabla \phi|^2 + \rho g x_3 \right\} \langle n', R \rangle d\Gamma \\ &+ \int_{\Gamma} \frac{\partial}{\partial n} \left\{ \left( \frac{1}{2} |\nabla \phi|^2 + \rho g x_3 \right) \langle \nabla b_{\Omega}, R \rangle \right\} v d\Gamma \\ &+ \int_{\Gamma} H \left( \frac{1}{2} |\nabla \phi|^2 + \rho g x_3 \right) \langle \nabla b_{\Omega}, R \rangle v d\Gamma \end{aligned}$$

We recall the by part integration formula:

$$\int_{\Omega} \text{Tr}(\mathcal{T}' \cdot DR) dx = - \int_{\Omega} \langle \vec{\text{Div}}(\mathcal{T}'), R \rangle dx + \int_{\Gamma} \langle \mathcal{T}' \cdot n, R \rangle d\Gamma$$

Then, taking  $\Psi$  (repectively  $R$ ) with compact support in  $\Omega^c$  (respectively in  $\Omega$ ) we get the following equations:

$$\begin{aligned} -\Delta \phi' &= 0 \quad \text{in } \Omega^c \\ -\vec{\text{Div}}(\mathcal{T}') &= 0 \quad \text{in } \Omega \end{aligned}$$

But

$$\begin{aligned} & \frac{\partial}{\partial n} \left\{ \left( \frac{1}{2} |\nabla \phi|^2 + \rho g x_3 \right) \langle \nabla b_{\Omega}, R \rangle \right\} \\ &= \langle n, \nabla \left\{ \left( \frac{1}{2} |\nabla \phi|^2 + \rho g x_3 \right) \langle \nabla b_{\Omega}, R \rangle \right\} \rangle \end{aligned}$$

$$= (< n, D^2\phi.\nabla\phi > + \rho g n_3) < n, R > + (\frac{1}{2}|\nabla\phi|^2 + \rho g x_3) < n, D^2b_\Omega.R + D^*R.n >$$

Notice that

$$< n, D^2b_\Omega.R > = < D^2b_\Omega.n, R > = 0, \text{ as } D^2b_\Omega.n = 0$$

Therefore, concerning the boundary conditions, and taking  $\Psi \in H^1(D)$  and  $R = 0$ , we obtain:

$$\frac{\partial}{\partial n}\phi' = \text{div}_\Gamma(v \nabla_\Gamma\phi)$$

In addition, taking  $\Psi = 0$  and  $R \in H^1(D, R^N)$  with  $DR.n = 0$  on  $\Gamma$ , we have:

$$< n, D^*R.n > = < DR.n, n > = 0.$$

Hence we have the following identity:

$$\begin{aligned} & \frac{\partial}{\partial n} \{ (\frac{1}{2}|\nabla\phi|^2 + \rho g x_3) < \nabla b_\Omega, R > \} \\ &= (< n, D^2\phi.\nabla\phi > + \rho g n_3) < n, R > \end{aligned}$$

Finally, we obtain the following variational problem at the boundary:

$$\begin{aligned} & \forall R \in H^1(\Gamma, R^N) \\ & \int_\Gamma < \mathcal{T}'.n, R > d\Gamma + \int_\Gamma \text{Tr}(\mathcal{T}.DR) v d\Gamma \\ &= \int_\Gamma < \nabla\phi', \nabla\phi > < n, R > d\Gamma \\ &+ \int_\Gamma \{ \frac{1}{2}|\nabla\phi|^2 + \rho g x_3 \} < n', R > d\Gamma \\ &+ \int_\Gamma (< n, D^2\phi.\nabla\phi > + \rho g n_3) < n, R > v d\Gamma \\ &+ \int_\Gamma H (\frac{1}{2}|\nabla\phi|^2 + \rho g x_3) < \nabla b_\Omega, R > v d\Gamma \end{aligned}$$

We have to perform a tangential by part integration in the term

$$\int_\Gamma \text{Tr}(\mathcal{T}.DR) v d\Gamma = \int_\Gamma \mathcal{T}_{i,j} \frac{\partial}{\partial x_j} R_i v d\Gamma = \int_\Gamma < \mathcal{T}_{i,}, \nabla R_i > v d\Gamma$$

But as for all  $i$  we have  $\frac{\partial}{\partial n} R_i = 0$ ,

$$\nabla R_i = \nabla_\Gamma R_i + \frac{\partial}{\partial n} R_i \vec{n} = \nabla_\Gamma R_i,$$

and

$$\begin{aligned} \int_\Gamma \text{Tr}(\mathcal{T}.DR) v d\Gamma &= \int_\Gamma < \mathcal{T}_{i,}, \nabla_\Gamma R_i > v d\Gamma = - \int_\Gamma \text{div}(v \mathcal{T}_{i,}) R_i d\Gamma \\ &= - \int_\Gamma < \vec{D}iv(v \mathcal{T}), R > d\Gamma, \end{aligned}$$

then we get the following boundary condition for the stress function :

$$\begin{aligned}
 & \forall R \in H^1(\Gamma, R^N) \\
 & \int_{\Gamma} \langle \mathcal{T}'.n, R \rangle d\Gamma = + \int_{\Gamma} \langle \vec{Div}(v\mathcal{T}), R \rangle d\Gamma \\
 & \quad + \int_{\Gamma} \langle \nabla\phi', \nabla\phi \rangle \langle n, R \rangle d\Gamma \\
 & \quad + \int_{\Gamma} \left\{ \frac{1}{2} |\nabla\phi|^2 + \rho g x_3 \right\} \langle n', R \rangle d\Gamma \\
 & \quad + \int_{\Gamma} (\langle n, D^2\phi \cdot \nabla\phi \rangle + \rho g n_3) \langle n, R \rangle v d\Gamma \\
 & \quad + \int_{\Gamma} H \left( \frac{1}{2} |\nabla\phi|^2 + \rho g x_3 \right) \langle \nabla b_{\Omega}, R \rangle v d\Gamma
 \end{aligned}$$

Therefore, we obtain

$$\begin{aligned}
 \mathcal{T}'.n &= \vec{Div}(v\mathcal{T}) + \langle \nabla\phi', \nabla\phi \rangle \vec{n} + \left\{ \frac{1}{2} |\nabla\phi|^2 + \rho g x_3 \right\} \vec{n}' \\
 &+ (\langle n, D^2\phi \cdot \nabla\phi \rangle + \rho g n_3) v \vec{n} + H \left( \frac{1}{2} |\nabla\phi|^2 + \rho g x_3 \right) v \vec{n}
 \end{aligned}$$

**4.1. Calculus of the tangent vector  $n'$ .** From [?], [?], [?], we know that in some neighborhood  $\mathcal{U}$  of  $\Sigma = \cup_{0 < s < s_1} \{s\} \times \partial\Omega_s$  the oriented distance function solves the convection equation

$$\frac{\partial}{\partial s} b_{\Omega_s} + \nabla b_{\Omega_s} \cdot V(s) op_{\Gamma_s} = 0$$

where  $p_{\Gamma_s} = I_d - b_{\Omega_s} \nabla b_{\Omega_s}$  is the projection mapping onto  $\Gamma_s$ .

Then we get

$$\begin{aligned}
 n' &:= \frac{\partial}{\partial s} (\nabla b_{\Omega_s})_{s=0} = \nabla \left( \frac{\partial}{\partial s} b_{\Omega_s} \right)_{s=0} = \left( \nabla (-\nabla b_{\Omega_s} \cdot V(s) op_{\Gamma_s}) \right)_{s=0} \\
 &= - \left( D^2 b_{\Omega_s} \cdot V(s) op_{\Gamma_s} \right)_{s=0} - \left( D^* (V(s) op_{\Gamma_s}) \cdot \nabla b_{\Omega_s} \right)_{s=0} \\
 s=0, x \in \Gamma, n'(x) &= - D^2 b_{\Omega}(x) \cdot V(0, x) - D_{\Gamma}^* V(0, x) \cdot n(x) \\
 &= - \nabla_{\Gamma} v(x)
 \end{aligned}$$

where again  $v(x) = \langle V(0, x), n(x) \rangle$  on  $\Gamma$  is the normal speed of the boundary.

As we have

$$\vec{Div}(\mathcal{T}) = 0 \text{ in } \Omega,$$

assuming the boundary  $\Gamma$  smooth we get that this equation holds true up to the boundary, so that the term  $\vec{Div}(v\mathcal{T})$  simplifies and we get

$$\vec{Div}(v\mathcal{T}) = v \vec{Div}(\mathcal{T}) + \mathcal{T} \cdot \nabla v.$$

Thus we have the following new expression:

$$\begin{aligned}
 \mathcal{T}'.n &= \mathcal{T} \cdot \nabla v + \langle \nabla_{\Gamma} \phi', \nabla_{\Gamma} \phi \rangle \vec{n} - \left\{ \frac{1}{2} |\nabla_{\Gamma} \phi|^2 + \rho g x_3 \right\} \nabla_{\Gamma} v \\
 &+ (\langle n, D^2\phi \cdot \nabla_{\Gamma} \phi \rangle + \frac{1}{2} H |\nabla_{\Gamma} \phi|^2 + (1 + H) \rho g n_3) v \vec{n} \quad (4.1)
 \end{aligned}$$

Regarding the term  $\nabla v$  on  $\Gamma$ , we have:

$$\nabla v = \nabla(\langle V(0), \nabla b_\Omega \rangle) = D^2 b_\Omega \cdot V(0) + D^* V(0) \cdot \nabla b_\Omega$$

Therefore it follows that

$$\langle \nabla v, n \rangle = \langle DV(0).n, n \rangle$$

and

$$\nabla v = \nabla_\Gamma v + \langle DV(0).n, n \rangle \vec{n}$$

Now using  $\mathcal{T}.n = p\vec{n} = (\frac{1}{2}|\nabla_\Gamma \phi|^2 + \rho g x_3)\vec{n}$ , equation (4.1) simplifies to:

$$\begin{aligned} \mathcal{T}'.n &= [\mathcal{T} - \{\frac{1}{2}|\nabla_\Gamma \phi|^2 + \rho g x_3\}].\nabla_\Gamma v + \langle \nabla_\Gamma \phi', \nabla_\Gamma \phi \rangle \vec{n} \\ &+ (\langle n, D^2 \phi \cdot \nabla_\Gamma \phi \rangle + \frac{1}{2}H |\nabla_\Gamma \phi|^2 + (1+H)\rho g x_3)v \vec{n} \\ &+ \langle DV(0).n, n \rangle (\frac{1}{2}|\nabla_\Gamma \phi|^2 + \rho g x_3) \vec{n} \end{aligned} \quad (4.2)$$

**4.2. The stress tensor  $\mathcal{T}_s \circ T_s$ .** Recall that  $T_s = \varphi_s \circ \varphi^{-1}$ , where  $\varphi_s = I + u_s$ , and that  $V(s) = \frac{\partial}{\partial s} T_s \circ T_s^{-1} = \frac{\partial}{\partial s} \varphi_s \circ \varphi_s^{-1}$ .

Then we get

$$V(s) = \frac{\partial}{\partial s} u_s \circ (I + u_s)^{-1}.$$

If we let

$$u' := (\frac{\partial}{\partial s} u_s)_{s=0}$$

then we obtain

$$V(0) = u' \circ (I + u)^{-1}$$

On the boundary  $\Gamma$  we have

$$v = \langle u' \circ (I + u)^{-1}, n \rangle$$

so that

$$\nabla_\Gamma v = \nabla_\Gamma(\langle u' \circ (I + u)^{-1}, n \rangle) = D_\Gamma^*(u' \circ (I + u)^{-1}).n + D^2 b_\Omega.(u' \circ (I + u)^{-1})_\Gamma$$

**Remark 4.1.** We design by  $K \in \mathcal{L}(H^{1/2}(\Gamma), H^{-1/2}(\Gamma))$  the self adjoint Dirichlet to Neuman operator at the boundary associated with harmoniques functions in  $\Omega$ . Then we get

$$\phi'|_\Gamma = K.(div_\Gamma(v \nabla_\Gamma \phi))$$

The stress tensor is the matrix

$$\mathcal{T}_s \circ T_s = (\frac{1}{\det(I + Du_s)}(I + Du_s). \Sigma(\sigma(u_s)).(I + D^* u_s)) \circ (I + u)^{-1} \quad (4.3)$$

where

$$\Sigma(\sigma(u_s)) = C_{\lambda, \mu}..(Du_s + D^* u_s + \frac{1}{2}Du_s.D^* u_s) \quad (4.4)$$

In (4.4) we assumed the four entries elasticity tensor to be governed by the Lamé coefficients.

Taking derivative w.r.t  $s$  in (4.3), we obtain:

$$\begin{aligned}
 \left( \left[ \frac{\partial}{\partial s} \mathcal{T}_s o \mathcal{T}_s \right]_{s=0} \right) o(I+u) &= - \frac{\operatorname{div}(u')}{\det(I+Du)} (I+Du).C_{\lambda,\mu}..(\sigma(u)).(I+D^*u) \\
 &+ \left( \frac{1}{\det(I+Du)} D(u').C_{\lambda,\mu}..(\sigma(u)).(I+D^*u) \right) \\
 &+ \left( \frac{1}{\det(I+Du)} (I+Du).C_{\lambda,\mu}..(\sigma').(I+D^*u) \right) \\
 &+ \left( \frac{1}{\det(I+Du)} (I+Du).C_{\lambda,\mu}..(\sigma(u)).D^*(u') \right)
 \end{aligned}$$

where

$$\sigma' = D(u') + D^*(u') + \frac{1}{2} (D(u').D^*u + Du.D^*(u'))$$

Now we let

$$\begin{aligned}
 \dot{\mathcal{T}} &= \left[ \frac{\partial}{\partial s} \mathcal{T}_s o \mathcal{T}_s \right]_{s=0} \\
 &= \mathcal{T}' + \mathbf{D}\mathcal{T}.(u' \circ (I+u)^{-1})
 \end{aligned}$$

where  $\mathbf{D}$  is a “new coming”: it is a three entries tensor, representing the gradient of the matrix  $\mathcal{T}$ . Its contraction with the vector  $(u' \circ (I+u)^{-1})$  gives the matrix  $\mathbf{D}\mathcal{T}.(u' \circ (I+u)^{-1})$ . Then we have

$$\begin{aligned}
 \mathcal{T}' &= \left\{ - \frac{\operatorname{div}(u')}{\det(I+Du)} (I+Du).C_{\lambda,\mu}..(\sigma(u)).(I+D^*u) \right\} o(I+u)^{-1} \\
 &+ \left\{ \left( \frac{1}{\det(I+Du)} D(u').C_{\lambda,\mu}..(\sigma(u)).(I+D^*u) \right) \right\} o(I+u)^{-1} \\
 &+ \left\{ \left( \frac{1}{\det(I+Du)} (I+Du).C_{\lambda,\mu}..(\sigma').(I+D^*u) \right) \right\} o(I+u)^{-1} \\
 &+ \left\{ \left( \frac{1}{\det(I+Du)} (I+Du).C_{\lambda,\mu}..(\sigma(u)).D^*(u') \right) \right\} o(I+u)^{-1} \\
 &\quad - \mathbf{D}\mathcal{T}.(u' \circ (I+u)^{-1})
 \end{aligned}$$

## 5. LINEARIZATION AROUND “REST”

The most “popular” framework (among mathematicians) consists in considering  $u = 0$ . With this assumption, we have the following simplification:

$$\mathcal{T}' = C_{\lambda,\mu}..(\sigma') - \mathbf{D}\mathcal{T}.(u' \circ (I+u)^{-1})$$

Since  $u = 0$ , we have that  $\mathcal{T} = 0$  and thus  $\mathbf{D}\mathcal{T} = 0$ . Moreover,

$$\sigma' = D(u' \circ (I+u)^{-1}) + D^*(u' \circ (I+u)^{-1})$$

Therefore

$$\mathcal{T}' = C_{\lambda,\mu}..(D(u' \circ (I+u)^{-1}) + D^*(u' \circ (I+u)^{-1}))$$

$$\mathcal{T}' = \lambda \det(D(u' \circ (I+u)^{-1})) I + \mu (D(u' \circ (I+u)^{-1}) + D^*(u' \circ (I+u)^{-1}))$$



So now we are in the classical linear elasticity framework:  $U := (u' \circ (I + u)^{-1})$  is the linearized displacement, while  $\bar{T} = T' = \lambda \det(DU) I + \mu (DU + D^*U)$  is the associated stress function.

**5.1. The linearization of the coupled fluid-structure problem around stress less steady structure.** We assume small variations around the rest state  $u = 0$ ,  $T = 0$  for the elastic body occupying the volume  $\Omega$  in  $D \subset R^3$ . The fluid speed  $v$  is steady, but not zero. We assume this flow to be irrotational so that  $v$  derives from an harmonic potential in  $\Omega^c = D \setminus \bar{\Omega}$ , that is  $v_s = \nabla \phi_s$ . From (4.2), with the following notation

$$\Phi = \phi',$$

we obtain the following system for the fluid-structure coupling (with  $\bar{T} = \lambda \det(DU) I + \mu (DU + D^*U)$ ):

$$\begin{aligned} \Delta \Phi &= 0 \text{ in } \Omega^c, \\ \vec{D}iv(\bar{T}) &= 0 \text{ in } \Omega, \\ \frac{\partial}{\partial n} \Phi &= - + \operatorname{div}_\Gamma(U.n \nabla_\Gamma \phi) \text{ on } \Gamma, \\ \bar{T}.n &= - \left\{ \frac{1}{2} |\nabla_\Gamma \phi|^2 + \rho g x_3 \right\} \cdot \nabla_\Gamma(U.n) + \langle \nabla_\Gamma \Phi, \nabla_\Gamma \phi \rangle \vec{n} \\ &\quad + (\langle n, D^2 \phi \cdot \nabla_\Gamma \phi \rangle + \frac{1}{2} H |\nabla_\Gamma \phi|^2 + (1 + H) \rho g n_3) U.n \vec{n} \\ &\quad + \langle DU.n, n \rangle \left( \frac{1}{2} |\nabla_\Gamma \phi|^2 + \rho g x_3 \right) \vec{n} \end{aligned} \quad (5.1)$$

Note that the coupling on the boundary interface  $\Gamma$  takes into account the mean curvature of the boundary  $H$ . This is an important point.

#### REFERENCES

- [1] R.A. Adams, “Sobolev Spaces”, Academic Press, New York-London, 1975.
- [2] G. Avalos and R. Triggiani, *Semigroup Well-posedness in the Energy Space of a Parabolic-Hyperbolic Coupled Stokes-Lame PDE System of Fluid-Structure Interaction*, Discrete and Continuous Dynamical Series S, Volume 2, Number 3, September 2009.
- [3] V. Barbu, Z. Grujic, I. Lasiecka, and A. Tuffaha, *Smoothness of Weak Solutions to a Nonlinear Fluid-structure Interaction Model* Indiana University Mathematics Journal, Vol. 57, No. 3, 2008.
- [4] L. Bociu, *Local and global wellposedness of weak solutions for the wave equation with nonlinear boundary and interior sources of supercritical exponents and damping*, Nonlin. Analysis TMA. (2008). [doi:10.1016/j.na.2008.11.062]
- [5] L. Bociu and I. Lasiecka, *Blow-up of weak solutions for the semilinear wave equations with nonlinear boundary and interior sources and damping* Applicationes Mathematicae, **35** (2008), 281–304.
- [6] L. Bociu and I. Lasiecka, *Uniqueness of Weak Solutions for the Semilinear Wave Equations with Supercritical Boundary/Interior Sources and Damping*, Discrete Contin. Dyn. Syst., **22** (2008), 835–860.
- [7] L. Bociu and I. Lasiecka, *Hadamard wellposedness for nonlinear wave equations with supercritical sources and damping*, Submitted to JDE, 2009.

- [8] L. Bociu, M. Rammaha and D. Toundykov, *On a wave equation with supercritical interior and boundary sources and damping terms*, Submitted to *Mathematische Nachrichten*, 2009.
- [9] S. Boisdérault and J.-P. Zolésio. Shape derivative of sharp functionals governed by Navier-Stokes flow. In *Partial differential equations (Praha, 1998)*, volume 406 of *Chapman & Hall/CRC Res. Notes Math.*, pages 49–63. Chapman & Hall/CRC, Boca Raton, FL, 2000.
- [10] S. Boisdérault and J.P. Zolésio. Boundary variations in the Navier-Stokes equations and Lagrangian functionals. In *Shape optimization and optimal design (Cambridge, 1999)*, volume 216 of *Lecture Notes in Pure and Appl. Math.*, pages 7–26. Dekker, New York, 2001.
- [11] P.G. Ciarlet, “Mathematical Elasticity Volume I: Three-dimensional Elasticity, North Holland, Amsterdam-New York-Oxford-Tokyo, 1988.
- [12] D. Coutand and S. Shkoller, *Motion of an Elastic Solid inside and Incompressible Viscous Fluid*, *Arch. Rational Mech. Anal.* 176 (2005), p. 25-102.
- [13] G. Da Prato and J.-P. Zolésio. Existence and optimal control for wave equation in moving domain. In *Stabilization of flexible structures (Montpellier, 1989)*, volume 147 of *Lecture Notes in Control and Inform. Sci.*, pages 167–190. Springer, Berlin, 1990.
- [14] Giuseppe Da Prato and Jean-Paul Zolésio. Boundary control for inverse free boundary problems. In *Boundary control and boundary variation (Sophia-Antipolis, 1990)*, volume 178 of *Lecture Notes in Control and Inform. Sci.*, pages 163–173. Springer, Berlin, 1992.
- [15] M.C. Delfour and J.P. Zolésio, “Shapes and Geometries: Analysis, Differential Calculus and Optimization, *Advances in Design and Control*, SIAM 2001.
- [16] Michel C. Delfour and Jean-Paul Zolésio. Shape analysis via oriented distance functions. *J. Funct. Anal.*, 123(1):129–201, 1994.
- [17] M. C. Delfour and J.-P. Zolésio. Dynamical free boundary problem for an incompressible potential fluid flow in a time-varying domain. *J. Inverse Ill-Posed Probl.*, 12(1):1–25, 2004.
- [18] Michel C. Delfour and Jean-Paul Zolésio. Boundary evolution. *Honoring Da Prato*, 4(1):29–52, 2006.
- [19] F. R. Desaint and Jean-Paul Zolésio. Manifold derivative in the Laplace-Beltrami equation. *J. Funct. Anal.*, 151(1):234–269, 1997.
- [20] Fabrice Desaint and Jean-Paul Zolésio. Shape boundary derivative for an elastic membrane. In *Advances in mathematical sciences: CRM’s 25 years (Montreal, PQ, 1994)*, volume 11 of *CRM Proc. Lecture Notes*, pages 481–491. Amer. Math. Soc., Providence, RI, 1997.
- [21] F. R. Desaint and J. P. Zolésio. Shape derivative for the Laplace-Beltrami equation. In *Partial differential equation methods in control and shape analysis (Pisa)*, volume 188 of *Lecture Notes in Pure and Appl. Math.*, pages 111–132. Dekker, New York, 1997.
- [22] Fabrice Desaint and Jean-Paul Zolésio. Sensitivity analysis of all eigenvalues of a symmetrical elliptic operator. In *Boundary control and variation (Sophia Antipolis, 1992)*, volume 163 of *Lecture Notes in Pure and Appl. Math.*, pages 141–160. Dekker, New York, 1994.
- [23] C. Grandmont, *Existence et unicite de solutions d’un probleme de couplage fluide-structure bidimensionnel stationnaire*, *C.R.Acad. Sci. Paris*, t. 326, Serie I (1998), p. 651-656.
- [24] C. Grandmont, *Existence for a Three-Dimensional Steady State Fluid-Structure Interaction Problem*, *J. math. fluid. mech.* 4 (2002), p. 76-94.
- [25] J. Sokołowski and J.-P. Zolésio. Shape design sensitivity analysis of plates and plane elastic solids under unilateral constraints. *J. Optim. Theory Appl.*, 54(2):361–382, 1987.

- [26] J. Sokołowski and J.-P. Zolésio. Shape sensitivity analysis of contact problem with prescribed friction. *Nonlinear Anal.*, 12(12):1399–1411, 1988.
- [27] Jan Sokołowski and Jean-Paul Zolésio. Shape sensitivity analysis of unilateral problems. *SIAM J. Math. Anal.*, 18(5):1416–1437, 1987.
- [28] M. Souli and J.-P. Zolésio. Shape derivative of discretized problems. *Comput. Methods Appl. Mech. Engrg.*, 108(3-4):187–199, 1993.
- [29] M. Souli and J. P. Zolésio. Finite element method for free surface flow problems. *Comput. Methods Appl. Mech. Engrg.*, 129(1-2):43–51, 1996.
- [30] M. Souli, J. P. Zolésio, and A. Ouahsine. Shape optimization for non-smooth geometry in two dimensions. *Comput. Methods Appl. Mech. Engrg.*, 188(1-3):109–119, 2000.
- [31] Jean-Paul Zolésio. Weak shape formulation of free boundary problems. *Ann. Scuola Norm. Sup. Pisa Cl. Sci. (4)*, 21(1):11–44, 1994.

*E-mail address:* lbociu2@math.unl.edu

CNRS-INLN AND INRIA, SOPHIA ANTIPOLIS, FRANCE, 06560

*E-mail address:* Jean-Paul.Zolesio@sophia.inria.fr